

Energy Eq - PNCOP @ Class 21

$$\frac{\partial \rho e}{\partial t} + \nabla \cdot (\rho \vec{e} \vec{v}) = -\nabla \cdot \vec{q} - \nabla \cdot (\vec{I} \cdot \vec{v}) - \nabla \cdot \vec{p} \vec{v} + \rho \vec{g} \cdot \vec{v}$$

C.S.; no K.E.; no Dissipation by μ ; no P.E.

$$\nabla \cdot (\rho \vec{e} \vec{v}) = -\nabla \cdot \vec{q} - \nabla \cdot \vec{p} \vec{v}$$

$$e = u = h - \frac{P}{\rho}$$

$$\nabla \cdot (\rho \vec{v} h) - \nabla \cdot (\vec{p} \vec{v}) = -\nabla \cdot \vec{q} - \cancel{\nabla \cdot (\vec{p} \vec{v})}$$

$$\boxed{\nabla \cdot (\rho \vec{v} h) = -\nabla \cdot \vec{q}}$$

$$\vec{q} = -\lambda \nabla T + \sum j_i h_i$$

$$\text{for } j_i = -\rho D_i \nabla Y_i, \quad D_i = \frac{\lambda}{P C_P} \quad (L e_i = 1)$$

$$\vec{q} = -\rho D \nabla h$$

$$\boxed{\nabla \cdot (\rho \vec{v} h) - \nabla \cdot (\rho D \nabla h) = 0}$$

for h_{gen} :

$$\rho \vec{v} \cdot \nabla h_{\text{gen}} - \nabla \cdot (\rho D \nabla h_{\text{gen}}) = - \sum h_{\text{gen}}^i \dot{m}_i'''$$

→ Shultz-Zeld.

Compare Species

$$\rho \vec{v} \cdot \nabla Y_i - \nabla \cdot (\rho D \nabla Y_i) = \dot{m}_i'''$$

brace

• Very Similar. (note sign)

$$\text{Note } \nabla h_{\text{gen}} = C_p \nabla T \quad \text{since } h_{\text{gen}} = \int_{T_f}^T C_p dT$$

These similarities → same soln form of PDE's for flames.

Lecture 21

Conserved Scalar

Last time we derived the following transport equation for enthalpy

$$\nabla \cdot (\rho v h) - \nabla \cdot (\rho D \nabla h) = 0$$

- SS
- no KLE, PLE, Visc, W_s , Radiation
- $Le_x = 1$

(Q): What indicates a conserved scalar here?

- Only Transport, no Sources, no Sinks
- Key enabler is $Le_x = 1$
- Also, can have an unsteady version of this.

* Other Conserved Scalars?

- Elemental mass fractions
- ↓
- Mixture fraction

* Conserved Scalars can significantly simplify analysis of combustion systems, - especially nonpremixed flames

- * - We have seen how we can represent h, T, Y_e as functions of ξ via assumptions like equilibrium. Then, if we knew ξ everywhere (via its transport equation) we could get $\phi(\xi)$ everywhere.
- This is routinely done in Turbulent non-premixed flames

ξ - Transport equation

Species Transport Eqn :

$$(1) \quad \frac{\partial \rho Y_e}{\partial t} + \nabla \cdot (\rho Y_e \mathbf{v}) - \nabla \cdot (\rho D \nabla Y_e) = \dot{m}_e'' \quad \text{Assumes } J = -\rho D_e \nabla Y_e$$

$$\xi = \frac{Z_k - Z_k^0}{Z_e - Z_k^0} \quad ; \quad Z_k = \sum_{i=1}^{N_{sp}} a_{k,i} \frac{M_k}{M_i} Y_i$$

$$D_e \equiv D \quad (\text{uniform } D)$$

- * $a_{k,i}, M_k, M_i, Z_k^0, (Z_e - Z_k^0)$ are all constants.

(2)

- Multiply (1) by $\alpha_{k,i} \frac{M_k}{M_i}$
- Sum over all i
- Pull the sum inside Derivatives.
- $\sum \alpha_{k,i} \frac{M_k}{M_i} \dot{m}_i''' = \dot{m}_k''' = 0$; Elements Don't react!

$$* \quad \frac{\partial \rho z_k}{\partial t} + \nabla \cdot (\rho z_k v) - \nabla \cdot (\rho D \nabla z_k) = 0$$

- Subtract z_k^0 (its constant \rightarrow pull inside Derivatives)
- $\therefore z_i - z_k^0$ (again const. \rightarrow "")

$$\boxed{\frac{\partial \rho \xi}{\partial t} + \nabla \cdot (\rho v \xi) - \nabla \cdot (\rho D \nabla \xi) = 0} = \text{Term (7.77)}$$

(7.78)
(7.79)

• Assumes $J = -\rho D_i \nabla Y_i$

• Assumes uniform $D_i \rightarrow D_i = D$

otherwise we can't pull \sum_i inside second ∇ in the Diffusive Term.

$\rightarrow \xi$ is a conserved scalar

Elements rearrange among Species via v_{xi} , but elements stay in ratio dictated by pure mixing

The Elements "Diffuse in Sync" so to speak.

• What to use for D ? usually use $\alpha \rightarrow \frac{\alpha}{D} = Le = 1$

* • If know any (1) conserved scalar, know all the others.

$$\xi \Rightarrow z_k \rightarrow h \quad \text{under given assumptions.}$$

Laminar flamelet equations

• Flames are usually thin \rightarrow 1-D \perp to flame sheet.

• 1-D species eqn: $\frac{\partial \rho Y_e}{\partial t} + \frac{\partial}{\partial x} (\rho Y_e v) - \frac{\partial}{\partial x} (\rho D \frac{\partial Y_e}{\partial x}) = \dot{m}'''$

Note: we said we can transport ξ , and if $Y_e = Y_e(\xi)$ then we can simplify combustion by transporting only ξ , and get $Y_e \approx Y_e(\xi)$.

* Convert the above eqn for $Y_e(t, x)$ to $Y_e(t, \xi)$

Consider the S.S. version $\rightarrow Y_e(x) \rightarrow Y_e(\xi)$

$$\begin{aligned}\xi = \xi(x) \rightarrow d\xi &= \frac{\partial \xi}{\partial x} dx \rightarrow \frac{d}{dx} = \frac{\partial \xi}{\partial x} \frac{d}{d\xi} \\ \rightarrow \frac{d\xi}{d\phi} &= \frac{\partial \xi}{\partial x} \frac{dx}{d\phi} \rightarrow \frac{d\phi}{dx} = \frac{d\xi}{\partial x} \frac{d\phi}{d\xi}\end{aligned}$$

Apply this:

$$\begin{aligned}&\left[\rho v \frac{\partial Y_e}{\partial x} \right] \underbrace{\frac{d\xi}{dx} \frac{d}{d\xi} (\rho Y_e v)}_{\rho v \frac{\partial \xi}{\partial x} \frac{\partial Y_e}{\partial \xi}} - \underbrace{\frac{d\xi}{dx} \frac{d}{d\xi} (\rho D \frac{d\xi}{dx} \frac{d}{d\xi} Y_e)}_{\rho D \left(\frac{d\xi}{dx} \right)^2 \frac{\partial^2 Y_e}{\partial \xi^2}} = \dot{m}''' \\ &\downarrow \\ &\left[\rho v \frac{\partial \xi}{\partial x} \frac{\partial Y_e}{\partial \xi} \right] - \underbrace{\frac{\partial \xi}{\partial x} \frac{\partial Y_e}{\partial \xi} \frac{\partial}{\partial \xi} \left(\rho D \frac{\partial \xi}{\partial x} \right)}_{\frac{\partial}{\partial x} \left(\frac{\partial \xi}{\partial x} \frac{\partial Y_e}{\partial \xi} \right)} - \rho D \left(\frac{\partial \xi}{\partial x} \right)^2 \frac{\partial^2 Y_e}{\partial \xi^2} = \dot{m}''' \\ &\downarrow \\ &\left[\frac{\partial \rho v \xi}{\partial x} \frac{\partial Y_e}{\partial \xi} \right] - \underbrace{\frac{\partial \xi}{\partial x} \frac{\partial Y_e}{\partial \xi} \left(\rho D \frac{\partial \xi}{\partial x} \right)}_{\frac{\partial}{\partial x} \left(\frac{\partial \xi}{\partial x} \frac{\partial Y_e}{\partial \xi} \right)} - \rho D \left(\frac{\partial \xi}{\partial x} \right)^2 \frac{\partial^2 Y_e}{\partial \xi^2} = \dot{m}''' \\ &\downarrow \\ &\left[\frac{\partial}{\partial x} \right] = 0 \quad \text{via } \xi \text{ transport equation.}\end{aligned}$$

$$\rightarrow \boxed{\rho D \left(\frac{\partial \xi}{\partial x} \right)^2 \frac{\partial^2 Y_e}{\partial \xi^2} = -\dot{m}'''}$$

* Unsteady version too. \rightarrow

(4)

$$D \left(\frac{\partial \xi}{\partial x} \right)^2 \frac{\partial^2 \gamma_e}{\partial \xi^2} = - \frac{m_1'''}{\rho}$$

Let $\chi = -2D \left(\frac{\partial \xi}{\partial x} \right)^2$

$$\rightarrow \boxed{\frac{\chi}{2} \frac{\partial^2 \gamma_e}{\partial \xi^2} = - \frac{m_1'''}{\rho}}$$

- χ is scalar Dissipation Rate
- $\chi (=) \frac{1}{S}$
- χ is a mixing timescale.
- Looks like $\frac{1}{\tau}$ in PSR eqns
- χ is treated as a parameter.

Solve these eqns for each χ .

1-D in ξ

$$\rightarrow Y_e = Y_e(\xi, \chi)$$

(Actually $\chi = \chi(\xi) = \chi_0 f(\xi)$ where $\chi_0 = \text{constant} \rightarrow$

$$Y_e = Y_e(\xi, \chi_0)$$



$$\chi = \chi_0 \exp(-2(\operatorname{erf}^{-1}(2\xi-1))^2) \quad \text{for 1-D opposed jet flames.}$$

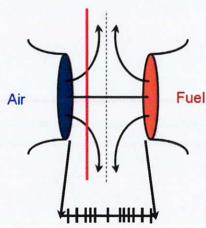
- if assume $\xi(x)$ is a tanh function instead of an erod function

$$\chi = \chi_0 (1 - (2\xi - 1)^2)^2$$

See PPT

Flamelet Modeling

- Flamelets transform physical coordinate to flame coordinate.
- Assumes unity Le



$$\rho \frac{\partial Y_i}{\partial t} = \rho v \frac{\partial Y_i}{\partial y} + \frac{\partial}{\partial y} \left(\rho D \frac{\partial Y_i}{\partial y} \right) + \omega_i$$

\downarrow

$$\frac{\partial Y_i}{\partial t} = \frac{\chi}{2} \frac{\partial^2 Y_i}{\partial \xi^2} + \omega_i / \rho$$

Define mixture fraction f by transport equation

$$* \quad \rho \frac{\partial \xi}{\partial t} + \rho v \frac{\partial \xi}{\partial y} - \frac{\partial}{\partial y} \left(\rho D \xi \frac{\partial \xi}{\partial y} \right) = 0$$

Species transport equation

$$\rho \frac{\partial Y_i}{\partial t} = \rho v \frac{\partial Y_i}{\partial y} + \frac{\partial}{\partial y} \left(\rho D \frac{\partial Y_i}{\partial y} \right) + \omega_i$$

Coordinate transformation

$$\frac{\partial}{\partial t} \rightarrow \frac{\partial}{\partial t} + \frac{\partial \xi}{\partial t} \frac{\partial}{\partial \xi} \quad \frac{\partial}{\partial y} \rightarrow \frac{\partial \xi}{\partial y} \frac{\partial}{\partial \xi}$$

Apply (*) and rearrange

$$\frac{\partial Y_i}{\partial t} = \frac{\chi}{2} \frac{\partial^2 Y_i}{\partial \xi^2} + \omega_i / \rho \quad \chi = 2D \left(\frac{\partial \xi}{\partial y} \right)^2$$

